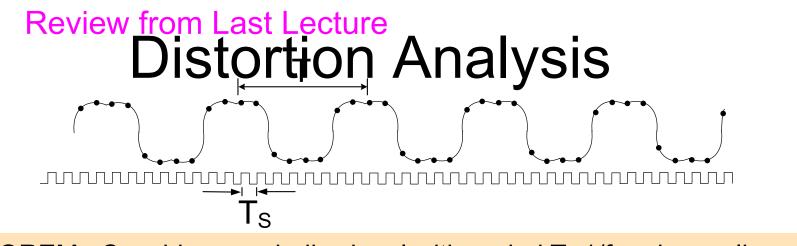
EE 505 Lecture 6

Spectral Analysis in Spectre

- Standard transient analysis
- Strobe period transient analysis

Addressing Spectral Analysis Challenges

- Problem Awareness
- Windowing
- Post-processing



THEOREM: Consider a periodic signal with period T=1/f and sampling period T_S=1/f_S. If N_P is an integer, x(t) is band limited to f_{MAX}, and f_s>2f_{max}, then $|A_m| = \frac{2}{N} |X(mN_P + 1)| \qquad 0 \le m \le h - 1$

and X(k)=0 for all k not defined above where $\langle X(k) \rangle_{k=0}^{N-1}$ is the DFT of the sequence $\langle x(kT_S) \rangle_{k=0}^{N-1}$ N=number of samples, N_P is the number of periods, and $h = Int \left(\frac{f_{MAX}}{f} - \frac{1}{N_P} \right)$ N_P an integer means N_P=N $\frac{T_S}{T}$ is an integer Spectral components of interest are $|A_m|$, m=0....h-1 Key Theorem central to Spectral Analysis that is widely used !!! and often "abused"

Considerations for Spectral Characterization



Tool Validation

•FFT Length

Importance of Satisfying Hypothesis

•Windowing

Tool Validation (MATLAB)

Likely does not cause significant errors for existing data converter spectral characterization applications

Likely can't attribute unexpected results in a design to MATLAB limitations for spectral characterization

Considerations for Spectral Characterization

Tool Validation

•FFT Length

Importance of Satisfying Hypothesis

•Windowing

Review from Last Lecture Considerations for Spectral Characterization FFT Length

- FFT Length does not significantly affect the computational noise floor
- Although not shown here yet, FFT length does reduce the <u>quantization</u> noise floor coefficients

If we assume $\mathsf{E}_{\mathsf{QUANT}}$ is fixed

$$\mathsf{E}_{QUANT} \cong \sqrt{\sum_{k=2}^{2^{n_{DFT}}} \mathsf{A}_{k}^{2}}$$

If the A_k 's are constant and equal

$$E_{QUANT} \cong A_k 2^{n_{DFT}/2}$$

Solving for A_k, obtain

$$A_k \cong \frac{E_{QUANT}}{2^{n_{DFT}/2}}$$

If input is full-scale sinusoid with only amplitude quantization with n-bit res,

$$\mathsf{E}_{\mathsf{QUANT}} \cong \frac{X_{LSB}}{\sqrt{12}} = \frac{X_{REF}}{\sqrt{3} \bullet 2^{n+1}}$$

Review from Last Lecture Considerations for Spectral Characterization FFT Length

$$\mathsf{E}_{\mathsf{QUANT}} \cong \frac{X_{LSB}}{\sqrt{12}} = \frac{X_{REF}}{\sqrt{3} \bullet 2^{n+1}}$$

Substituting for $\mathsf{E}_{\mathsf{QUANT}}$, obtain

$$A_{k} \cong \frac{X_{REF}}{\sqrt{3} \cdot 2^{n+1} 2^{n_{DFT}/2}}$$

This value for A_k thus decreases with the length of the DFT window

Example: if n=16, n_{DFT} =12 (4096 pt transform), and X_{REF} =1V, then A_k=6.9E-8V (-143dB),

(Note A_k >> computational noise for all practical n, n_{DFT})

Review from Last Lecture Considerations for Spectral Characterization

- Tool Validation
- FFT Length
- Importance of Satisfying Hypothesis
 - NP is an integer
 - Band-limited excitation
- Windowing

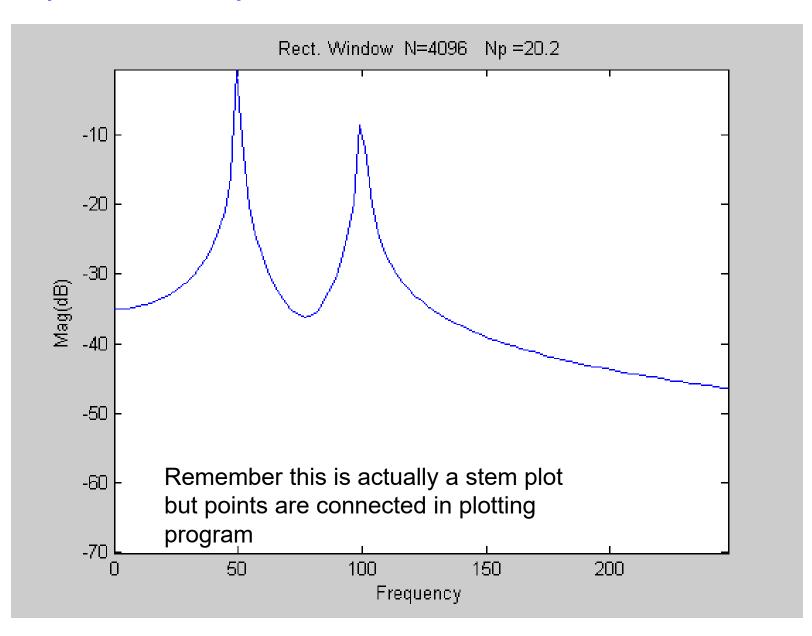
Example

WLOG assume f_{SIG} =50Hz $V_{IN} = sin(\omega t) + 0.5 sin(2\omega t)$ $\omega = 2\pi f_{SIG}$

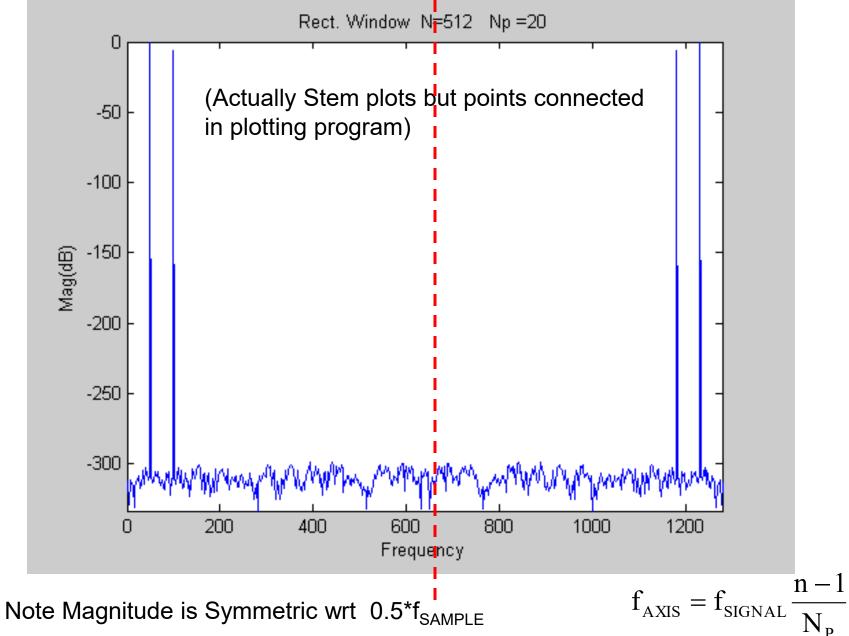
Consider N_P =20.2 N=4096

Recall 20log₁₀(0.5)=-6.0205999

Review from Last Lecture Spectral Response

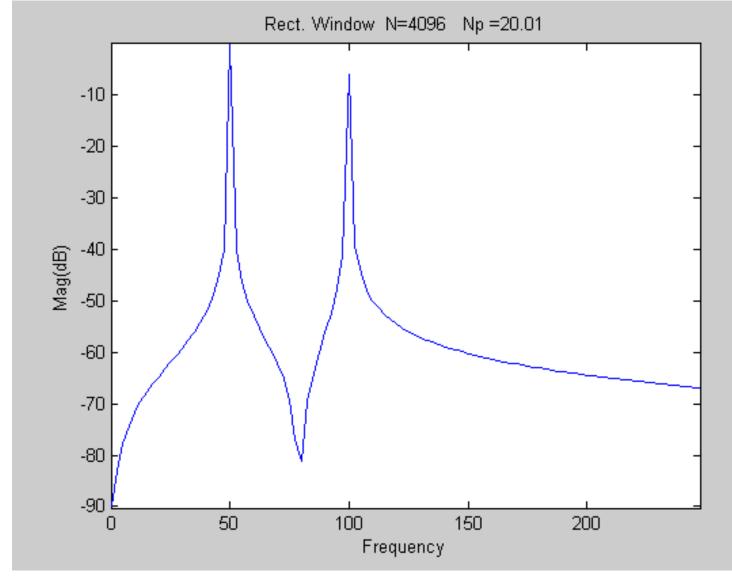


Spectral Response (expressed in dB)



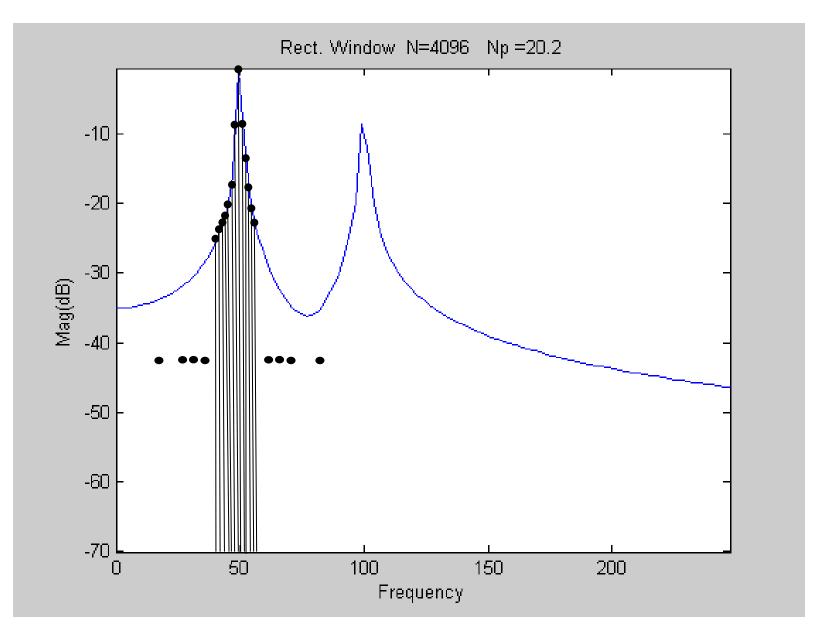
Review from last lecture

Spectral Response with Non-coherent Sampling



(zoomed in around fundamental)

Spectral Response



Fundamental will appear at position 1+Np = 21

Columns 1 through 7

-35.0366 -35.0125 -34.9400 -34.8182 -34.6458 -34.4208 -34.1403

Columns 8 through 14

-33.8005 -33.3963 -32.9206 -32.3642 -31.7144 -30.9535 -30.0563

Columns 15 through 21

-28.9855 -27.6830 -26.0523 -23.9155 -20.8888 -15.8561 **-0.5309**

Columns 22 through 28

-12.8167 -20.1124 -24.2085 -27.1229 -29.4104 -31.2957 -32.8782

Columns 29 through 35

-34.1902 -35.2163 -35.9043 -36.1838 -35.9965 -35.3255 -34.1946

Note there is a dramatic increase in the noise floor and a significant change in and spreading of the fundamental!!

kth harmonic will appear at position 1+k•Np

Columns 36 through 42 -32.6350 -30.6397 -28.1125 -24.7689 -19.7626 -8.5639 -11.7825 Columns 43 through 49 -20.0158 -23.9648 -26.5412 -28.4370 -29.9279 -31.1519 -32.1874 Columns 50 through 56 -33.0833 -33.8720 -34.5759 -35.2113 -35.7902 -36.3218 -36.8133 Columns 57 through 63 -37.2703 -37.6974 -38.0984 -38.4762 -38.8336 -39.1725 -39.4949 Columns 64 through 70

-39.8024 -40.0963 -40.3778 -40.6479 -40.9076 -41.1576 -41.3987

kth harmonic will appear at position 1+k•Np

Columns 36 through 42 -32.6350 -30.6397 -28.1125 -24.7689 -19.7626 -8.5639 -11.7825 Columns 43 through 49 -20.0158 -23.9648 -26.5412 -28.4370 -29.9279 -31.1519 -32.1874 Columns 50 through 56 -33.0833 -33.8720 -34.5759 -35.2113 -35.7902 -36.3218 -36.8133 Columns 57 through 63 -37.2703 -37.6974 -38.0984 -38.4762 -38.8336 -39.1725 -39.4949 Columns 64 through 70

-39.8024 -40.0963 -40.3778 -40.6479 -40.9076 -41.1576 -41.3987

Observations

- Modest change in sampling window of 0.2 out of 20 periods (1%) results in a big error in both fundamental and harmonic
- More importantly, dramatic raise in the "noise floor" !!! (from over -300dB to only -12dB)

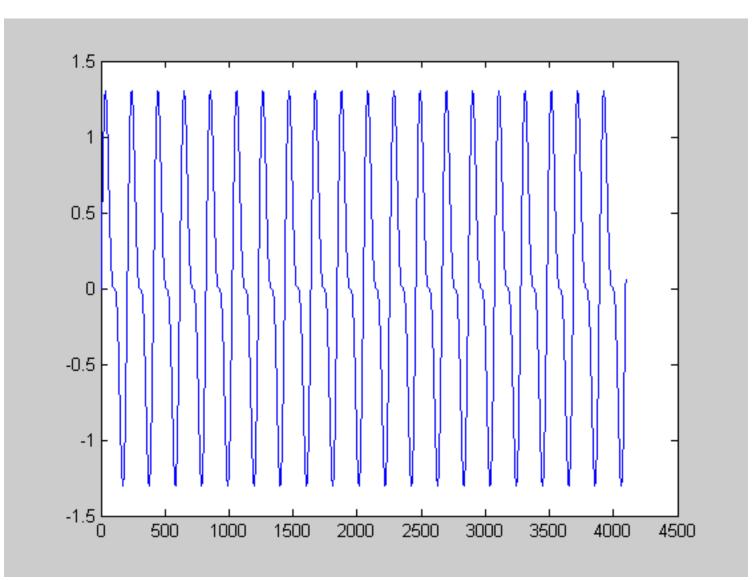
Example

WLOG assume f_{SIG} =50Hz $V_{IN} = sin(\omega t) + 0.5 sin(2\omega t)$ $\omega = 2\pi f_{SIG}$

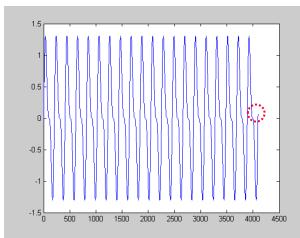
Consider N_P=20.01 N=4096

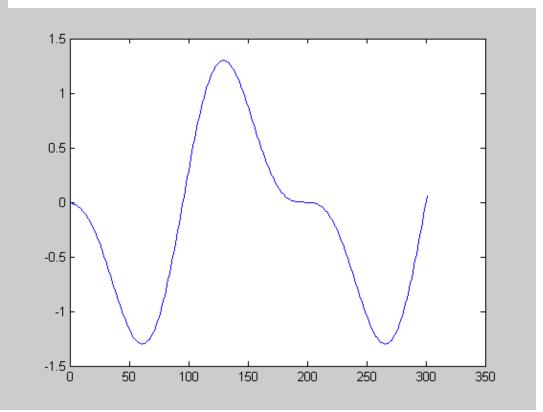
Deviation from hypothesis is .05% of the sampling window

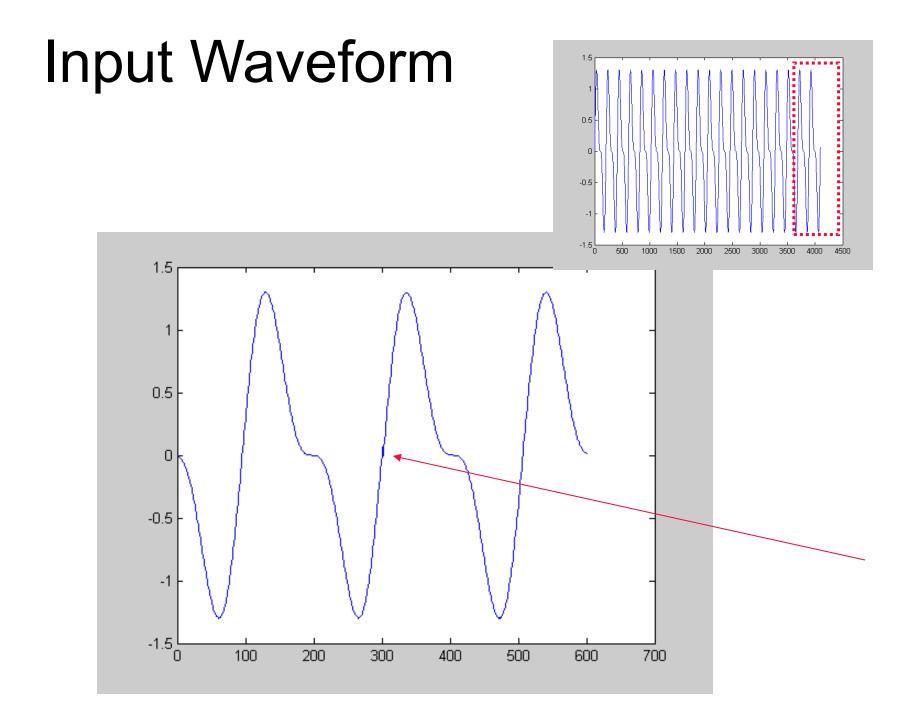
Input Waveform

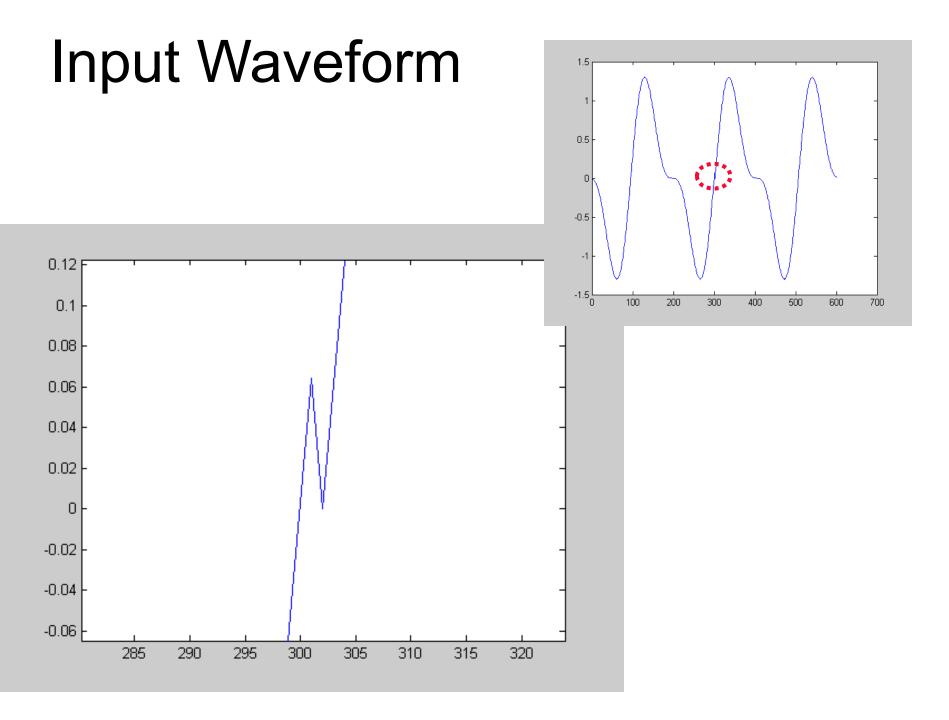


Input Waveform

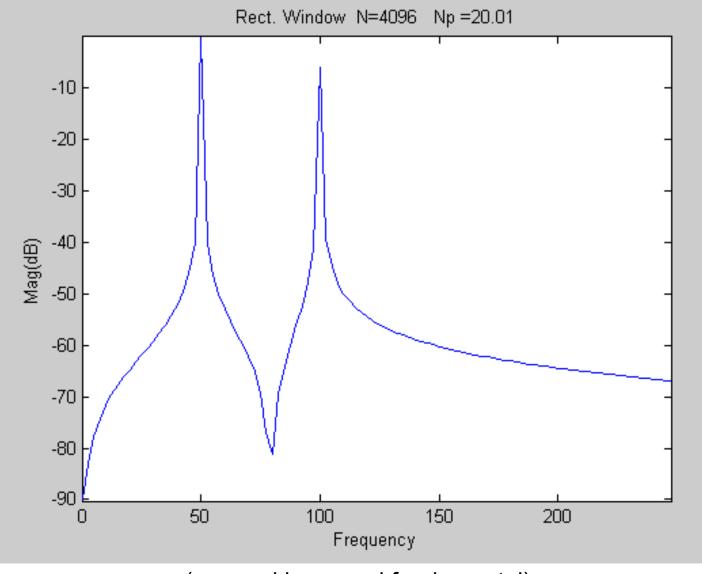








Spectral Response with Non-Coherent Sampling



(zoomed in around fundamental)

Fundamental will appear at position 1+Np = 21

Columns 1 through 7

-89.8679 -83.0583 -77.7239 -74.2607 -71.6830 -69.5948 -67.8044

Columns 8 through 14

-66.2037 -64.7240 -63.3167 -61.9435 -60.5707 -59.1642 -57.6859

Columns 15 through 21

-56.0866 -54.2966 -52.2035 -49.6015 -46.0326 -40.0441 -0.0007

Columns 22 through 28

-40.0162 -46.2516 -50.0399 -52.8973 -55.3185 -57.5543 -59.7864 Columns 29 through 35

-62.2078 -65.1175 -69.1845 -76.9560 -81.1539 -69.6230 -64.0636

kth harmonic will appear at position 1+k•Np

Columns 36 through 42

-59.9172 -56.1859 -52.3380 -47.7624 -40.9389 -6.0401 -39.2033

Observations

- Modest change in sampling window of 0.01 out of 20 periods (.05%) still results in a modest error in both fundamental and harmonic
- More importantly, substantial raise in the computational noise floor !!! (from over 300dB to only -40dB)
- Errors at about the 6-bit level !

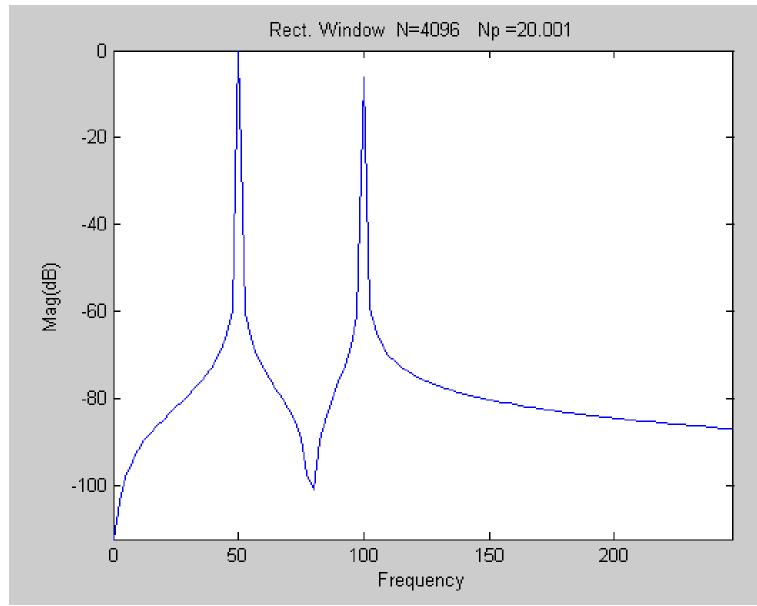
Example

WLOG assume f_{SIG} =50Hz $V_{IN} = sin(\omega t) + 0.5 sin(2\omega t)$ $\omega = 2\pi f_{SIG}$

Consider N_P=20.001 N=4096

Deviation from hypothesis is .005% of the sampling window

Spectral Response with Non-coherent Sampling



(zoomed in around fundamental)

Fundamental will appear at position 1+Np = 21

Columns 1 through 7

-112.2531 -103.4507 -97.8283 -94.3021 -91.7015 -89.6024 -87.8059

Columns 8 through 14

-86.2014 -84.7190 -83.3097 -81.9349 -80.5605 -79.1526 -77.6726

Columns 15 through 21

-76.0714 -74.2787 -72.1818 -69.5735 -65.9919 -59.9650 0.0001

Columns 22 through 28

-60.0947 -66.2917 -70.0681 -72.9207 -75.3402 -77.5767 -79.8121

Columns 29 through 35

-82.2405 -85.1651 -89.2710 -97.2462 -101.0487 -89.5195 -83.9851

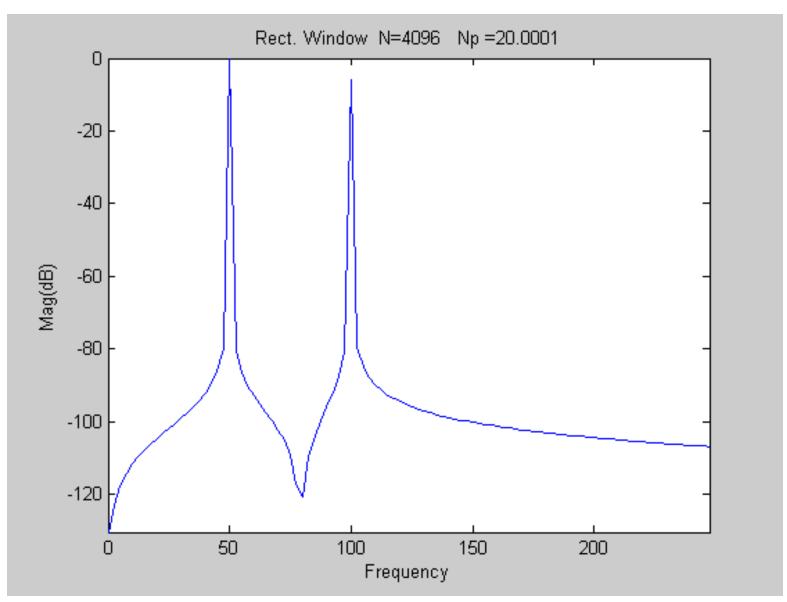
kth harmonic will appear at position 1+k•Np

Columns 36 through 42 -79.8472 -76.1160 -72.2601 -67.6621 -60.7642 -6.0220 -59.3448 Columns 43 through 49 -64.8177 -67.8520 -69.9156 -71.4625 -72.6918 -73.7078 -74.5718 Columns 50 through 56 -75.3225 -75.9857 -76.5796 -77.1173 -77.6087 -78.0613 -78.4809 Columns 57 through 63 -78.8721 -79.2387 -79.5837 -79.9096 -80.2186 -80.5125 -80.7927

Observations

- Modest change in sampling window of 0.01 out of 20 periods (.005%) results in a small error in both fundamental and harmonic
- More importantly, substantial raise in the computational noise floor !!! (from over 300dB to only -60dB)
- Errors at about the 10-bit level !

Spectral Response with Non-coherent sampling



(zoomed in around fundamental)

Fundamental will appear at position 1+Np = 21

Columns 1 through 7

-130.4427 -123.1634 -117.7467 -114.2649 -111.6804 -109.5888 -107.7965

Columns 8 through 14

-106.1944 -104.7137 -103.3055 -101.9314 -100.5575 -99.1499 -97.6702

Columns 15 through 21

-96.0691 -94.2764 -92.1793 -89.5706 -85.9878 -79.9571 0.0000

Columns 22 through 28

-80.1027 -86.2959 -90.0712 -92.9232 -95.3425 -97.5788 -99.8141

Columns 29 through 35

-102.2424 -105.1665 -109.2693 -117.2013 -120.8396 -109.4934 -103.9724

kth harmonic will appear at position 1+k•Np

Columns 36 through 42 -99.8382 -96.1082 -92.2521 -87.6522 -80.7470 -6.0207 -79.3595 Columns 43 through 49 -84.8247 -87.8566 -89.9190 -91.4652 -92.6940 -93.7098 -94.5736 Columns 50 through 56 -95.3241 -95.9872 -96.5810 -97.1187 -97.6100 -98.0625 -98.4821 Columns 57 through 63 -98.8732 -99.2398 -99.5847 -99.9107 -100.2197 -100.5135 -100.7937 Columns 64 through 70

Observations

- Modest change in sampling window of 0.001 out of 20 periods (.0005%) results in a small error in both fundamental and harmonic
- More importantly, substantial raise in the computational noise floor !!! (from over 300dB to only -80dB)
- Errors at about the 13-bit level !

Considerations for Spectral Characterization

- Tool Validation
- FFT Length
- Importance of Satisfying Hypothesis
 - NP is an integer
 - Band-limited excitation
- Windowing



Stay Safe and Stay Healthy !

FFT Examples

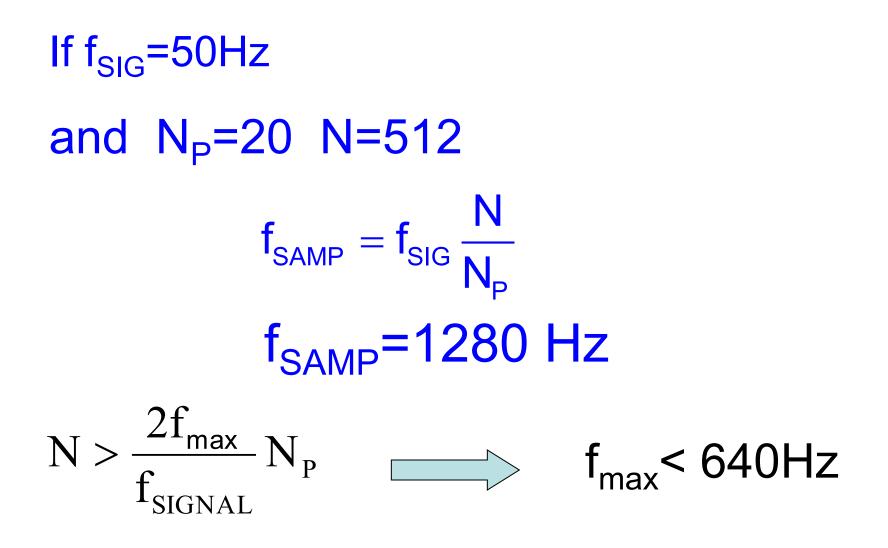
Recall the theorem that provided for the relationship between the DFT terms and the Fourier Series Coefficients required

1. The sampling window be an integral number of periods

$$N > \frac{2f_{max}}{f_{signal}} N_{p}$$

> 2.

Example



Example

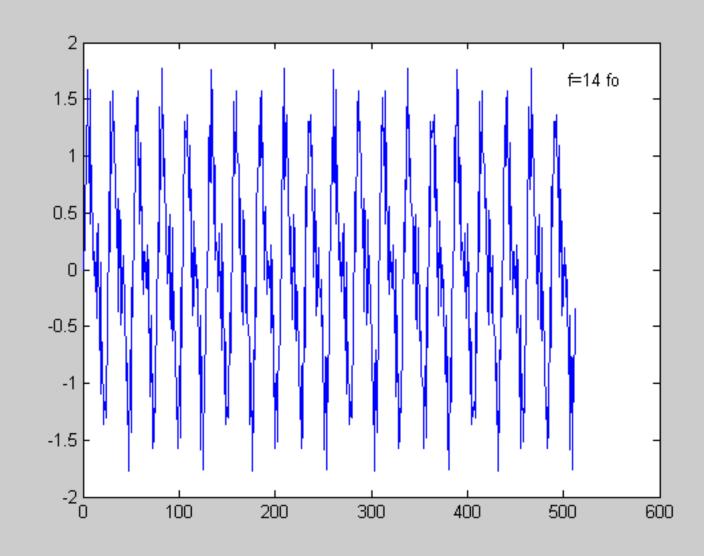
Consider N_P =20 N=512 If f_{SIG} =50Hz

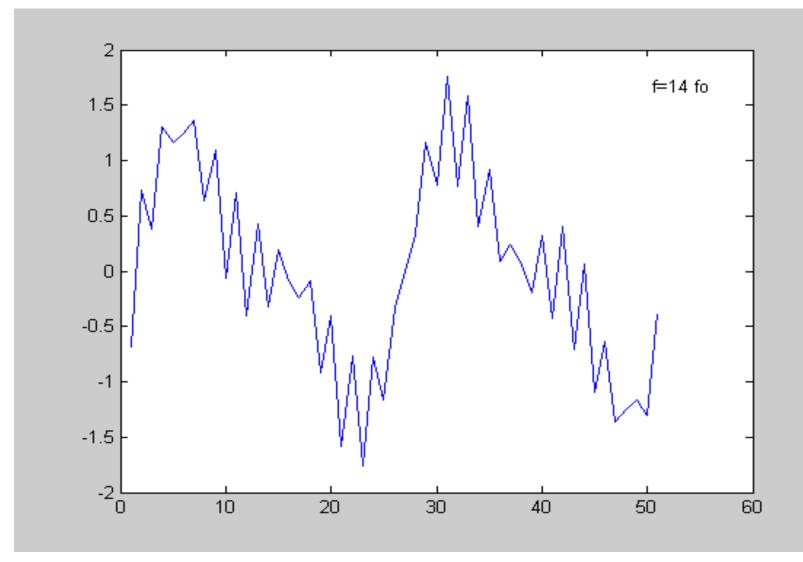
 $V_{IN} = sin(\omega t) + 0.5 sin(2\omega t) + 0.5 sin(14\omega t)$

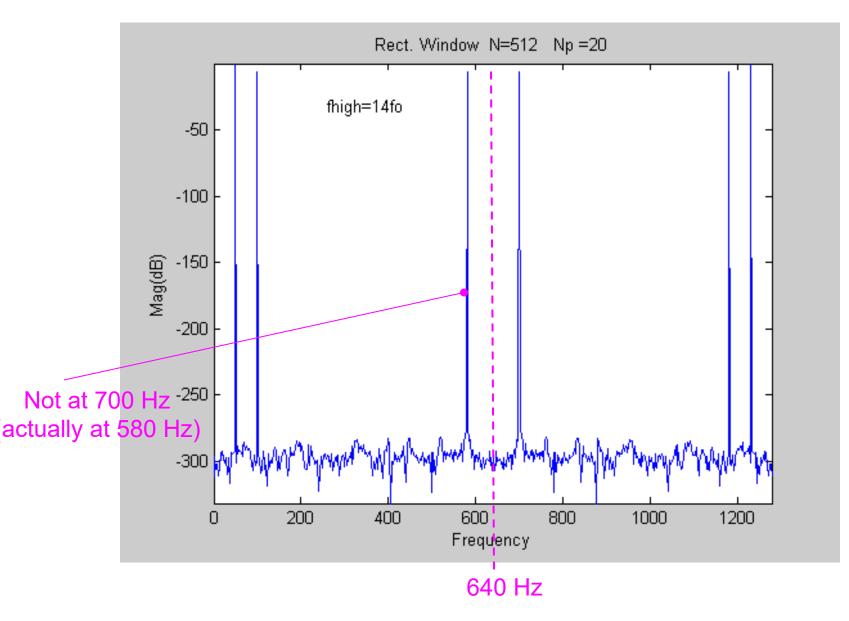
$$\omega = 2\pi f_{SIG}$$

(i.e. a component at 700 Hz which violates the band limit requirement)

Recall 20log₁₀(0.5)=-6.0205999







Effects of High-Frequency Spectral Components f_{hiah} =14fo

Columns 1 through 7

-296.9507 -311.9710 -302.4715 -302.1545 -310.8392 -304.5465 -293.9310

Columns 8 through 14

-299.0778 -292.3045 -297.0529 -301.4639 -297.3332 -309.6947 -308.2308

Columns 15 through 21

-297.3710 -316.5113 -293.5661 -294.4045 -293.6881 -292.6872 -0.0000

Columns 22 through 28

-301.6889 -288.4812 -292.5621 -292.5853 -294.1383 -296.4034 -289.5216

Columns 29 through 35

-285.9204 -292.1676 -289.0633 -292.1318 -290.6342 -293.2538 -296.8434

Effects of High-Frequency Spectral Components f_{high}=14fo

Columns 36 through 42

-301.7087 -307.2119 -295.1726 -303.4403 -301.6427 -6.0206 -295.3018

Columns 43 through 49

-298.9215 -309.4829 -306.7363 -293.0808 -300.0882 -306.5530 -302.9962

Columns 50 through 56

-318.4706 -294.8956 -304.4663 -300.8919 -298.7732 -301.2474 -293.3188

Aliased components at $f_{alias} = f_{sample} - f$

 $f_{alias} = 1280 - 700 = 580 Hz$

thus position in sequence = $1 + N \frac{f_{alias}}{f_{sample}} = 1 + 512 \frac{580}{1280} = 233$

Columns 225 through 231

-296.8883 -292.8175 -295.8882 -286.7494 -300.3477 -284.4253 -282.7639

Columns 232 through 238

-273.9840 -6.0206 -274.2295 -284.4608 -283.5228 -297.6724 -291.7545

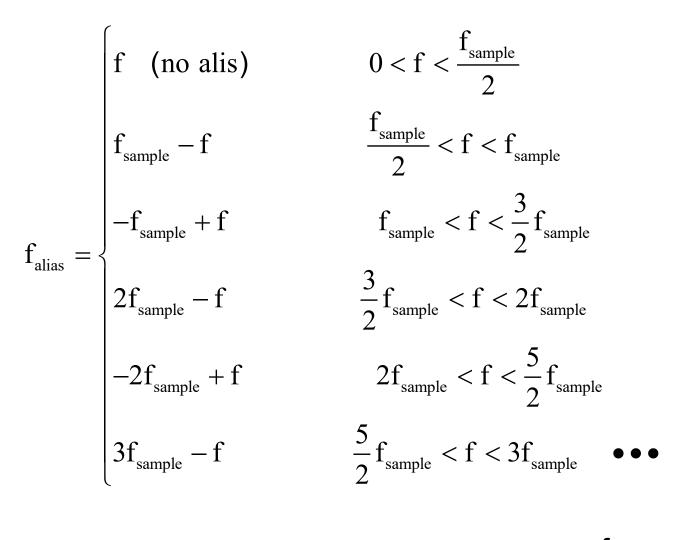
Columns 239 through 245

-299.1299 -305.8361 -295.1772 -295.1670 -300.2698 -293.6406 -304.2886

Columns 246 through 252

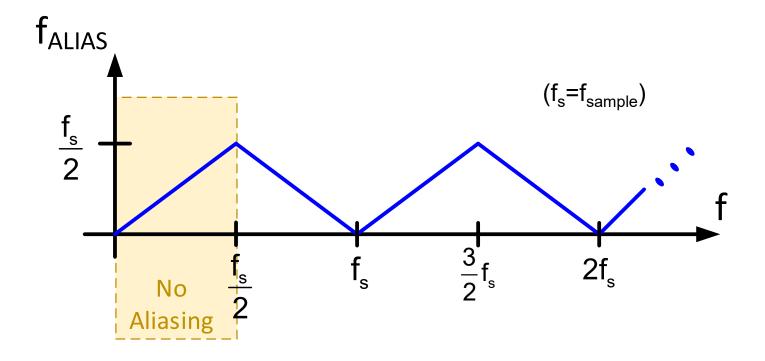
-302.0233 -306.6100 -297.7242 -305.4513 -300.4242 -298.1795 -299.0956

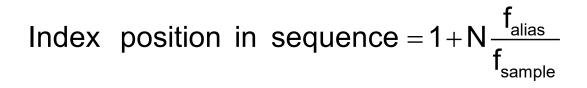
Alias frequency and Index Position



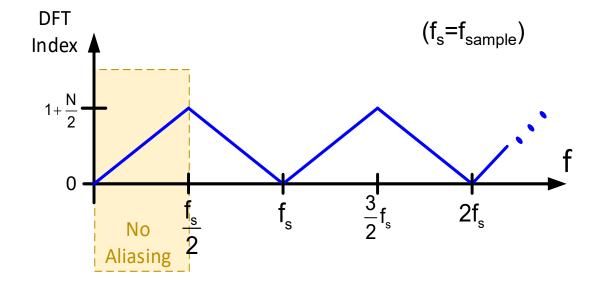
Index position in sequence = $1 + N \frac{f_{alias}}{f_{sample}}$

Alias frequency and Index Position

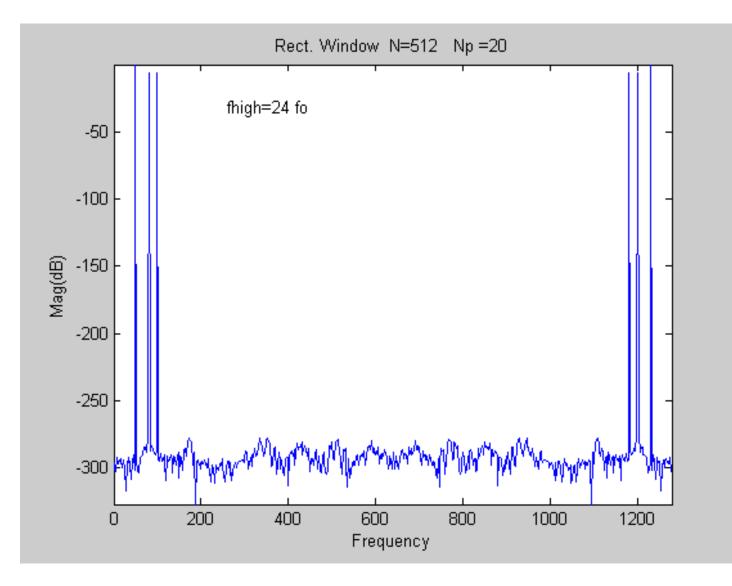


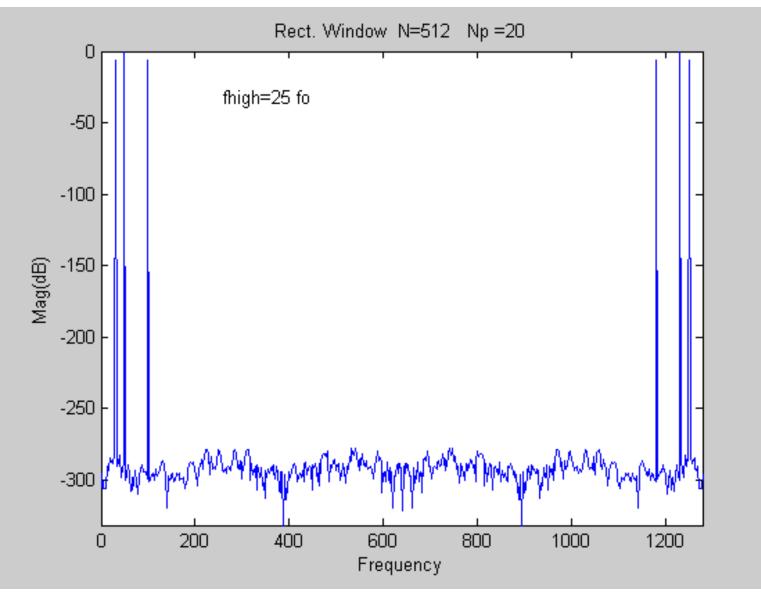


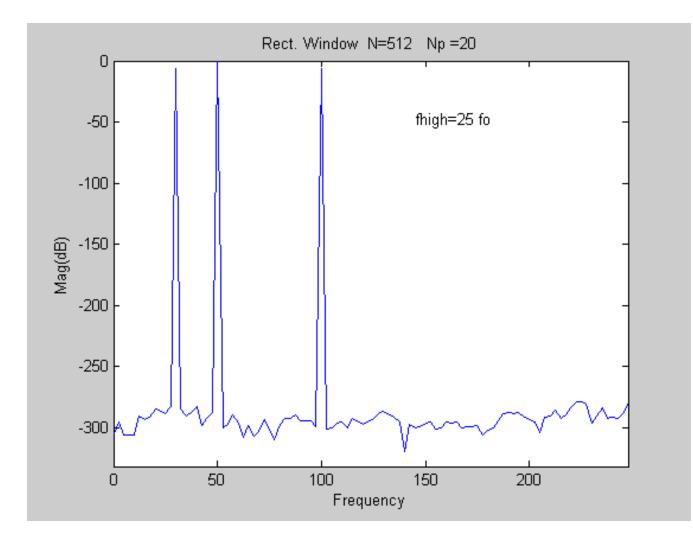
Alias frequency and Index Position



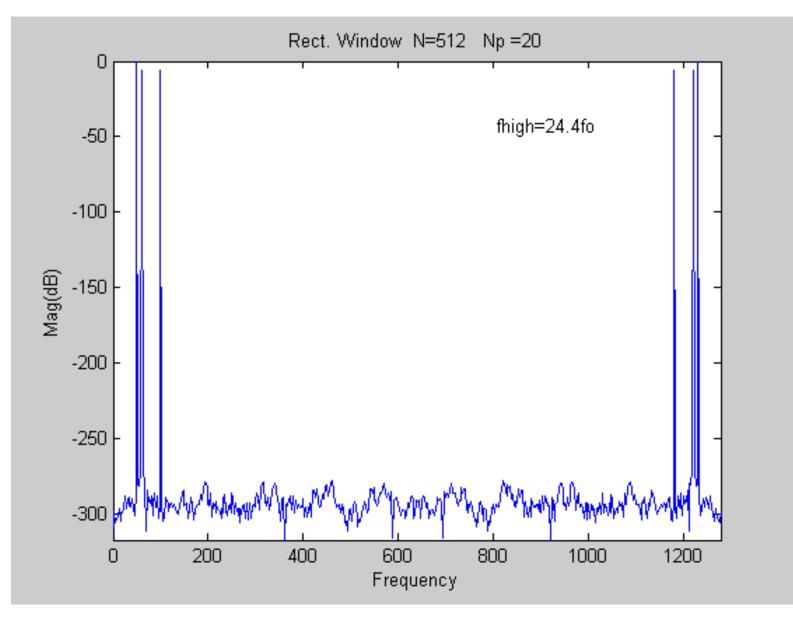
Index position in sequence = $1 + N \frac{f_{alias}}{f_{sample}}$

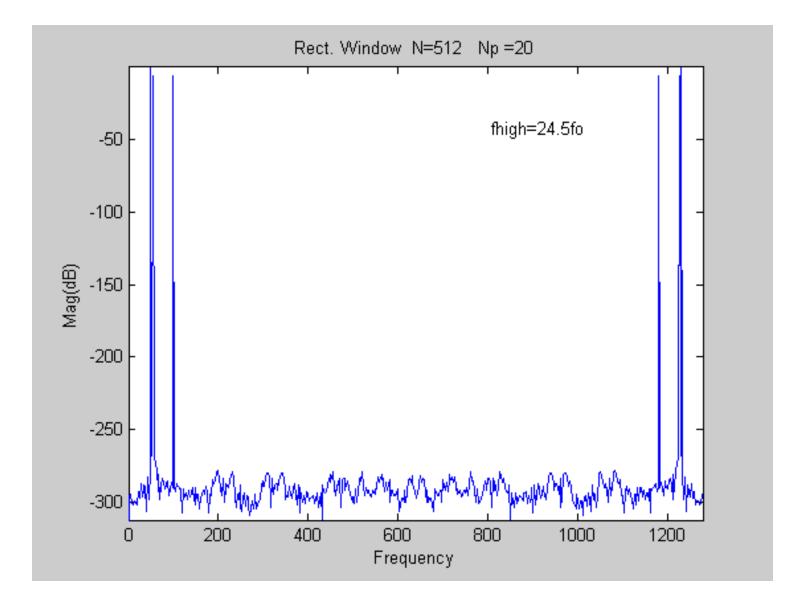






(zoomed in around fundamental)

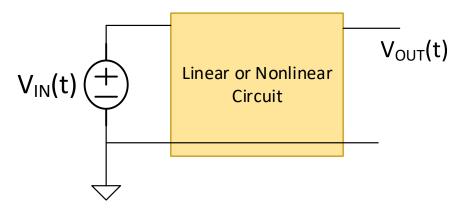




Observations

- Aliasing will occur if the band-limited part of the hypothesis for using the DFT is not satisfied
- Modest aliasing will cause high frequency components that may or may not appear at a harmonic frequency
- More egregious aliasing can introduce components near or on top of fundamental and lower-order harmonics
- Important to avoid aliasing if the DFT is used for spectral characterization

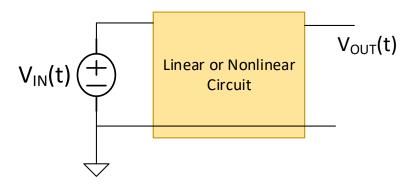
The transient simulation results obtained with almost all circuit simulators are almost always wrong!



If $V_{IN}=V_m sin(\omega t)$, the probability that any output for any linear or nonlinear circuit is the correct value is likely 0

The suppliers of all commercial circuit simulators know that their simulators almost never provide the correct solution for transient analysis in even simple circuits

But the solutions provided are often very good approximations to the actual solution



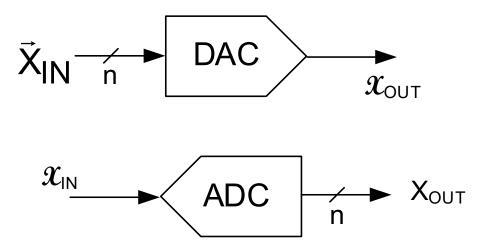
Obtaining an exact result for a transient simulation is an extremely challenging problem and even obtaining very good results have required major efforts by the CAD community for many decades

It is highly unlikely that the goal of any CAD tool vendor is to provide the exact transient solution

So what is likely the goal of a CAD tool vendor when developing tools to provide the transient response of a circuit?

Conjecture: To provide solutions that are good enough to convince customers to spend money to use the simulator !

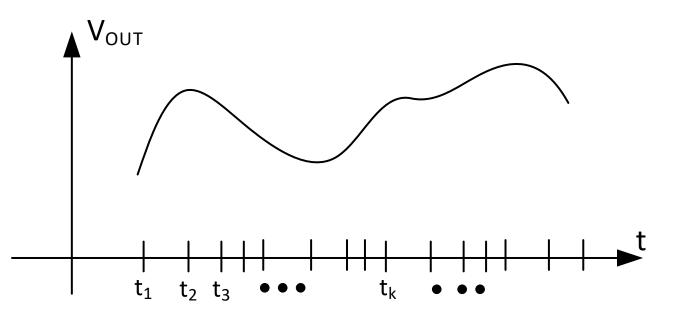
Is this a good goal that well-serves the customer?



There are numerous quirks that become issues when simulating ADCs of DACs , particularly when the specifications are demanding

Will discuss one of these quirks associated with spectral characterization today

Time steps in transient simulations

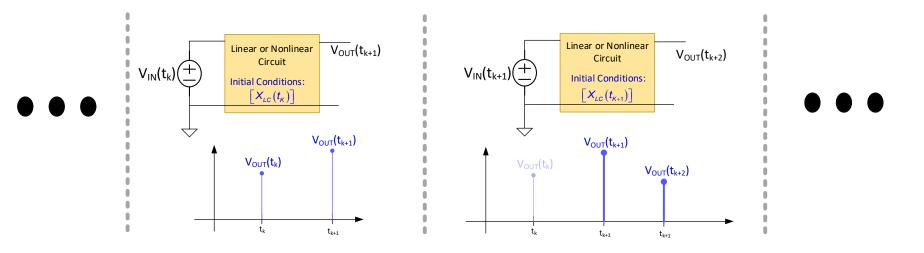


Transient analysis in SPICE involves breaking the simulation time interval into short sub-intervals of length $\hat{t}_k = t_{k+1} - t_k$

The solution involves using the calculated output at time t_k as the input at time t_{k+1}

The time steps are intentionally not uniform to provide reasonable tradeoffs between simulation time and accuracy

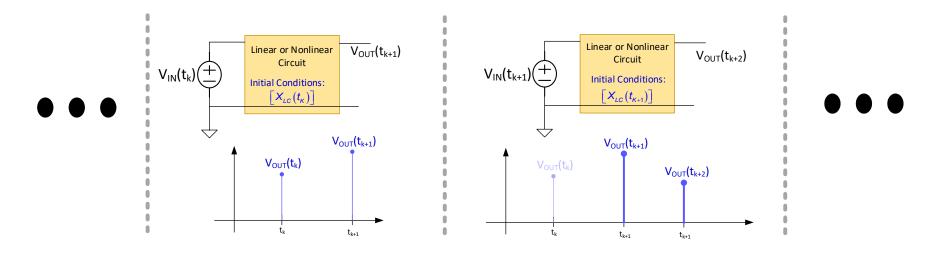
Transient Simulation Approach in Simulators



 $\begin{bmatrix} X_{LC}(t) \end{bmatrix}$ is the vector of the instantaneous value of all capacitor voltages and all inductor currents

- Transient simulations are decomposed into a sequence of individual problems where the output of all energy storage elements at step k serves as the initial condition (not initial guess) of all energy storage elements at step k+1
- Simulator attempts to conserve charge in each simulation step. This is a key concept that must be incorporated for consistency in any circuit simulator when Ls and Cs are included in schematic.

Transient Simulation Approach in Simulators



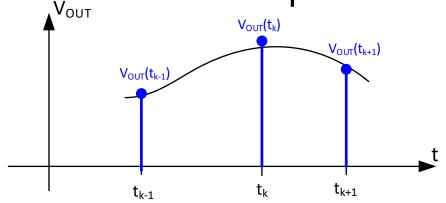
Simulator attempts to conserve charge in each simulation step (KCL and KVL)

Basic physical principle that is integral to any transient simulation of circuits with energy storage elements: CHARGE IS CONSERVED !!

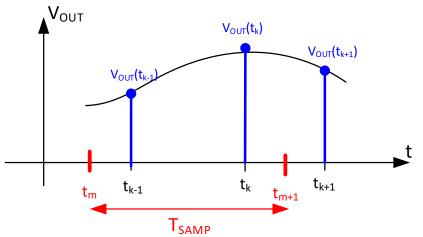
Is charge conserved in a circuit simulator when doing transient simulations?

No! It is only conserved locally (in individual time intervals) so major divergence can occur in some extreme situations due to accumulative round off effects

Transient Simulation For Spectral Characterization

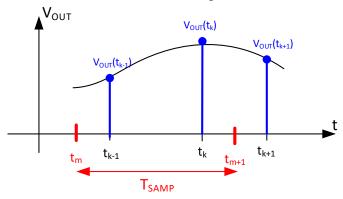


Normal time-stepping algorithm is used to obtain transient response



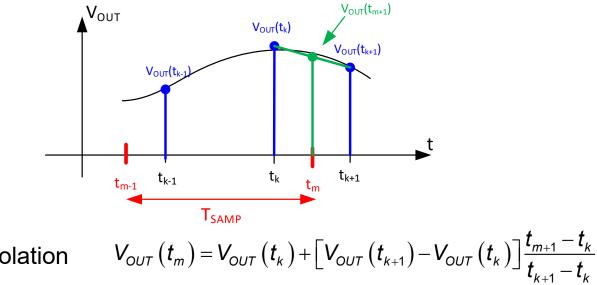
DFT requires output at precisely uniformly spaced predetermined points, t_m, t_{m+1} ... These points are almost never coincident with the time-stepping points !

Transient Simulation For Spectral Characterization



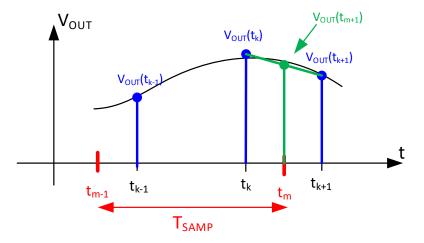
So how does the simulator generate outputs at the required time points ?

It interpolates ! Exact interpolation algorithm may vary from vendor to vendor



For linear interpolation

Transient Simulation For Spectral Characterization

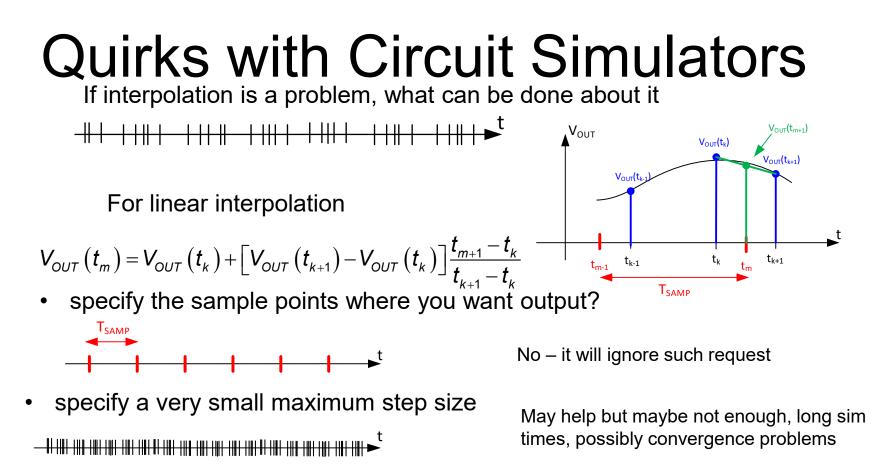


For linear interpolation

$$V_{OUT}(t_{m}) = V_{OUT}(t_{k}) + \left[V_{OUT}(t_{k+1}) - V_{OUT}(t_{k})\right] \frac{t_{m+1} - t_{k}}{t_{k+1} - t_{k}}$$

What errors are introduced in determining $V_{OUT}(t_m)$?

- Errors in calculating V_{OUT}(t_k) (most problematic for long simulations with multiple energy storage elements) (may not be particularly problematic for spectral characterization since N_P often not too long) (must simulate long enough for natural response to die out if ALL initial conditions are not correctly set)
- Errors associated with interpolation $V_{OUT}(t_k)$



• modify time stepping algorithm to include desired sample points

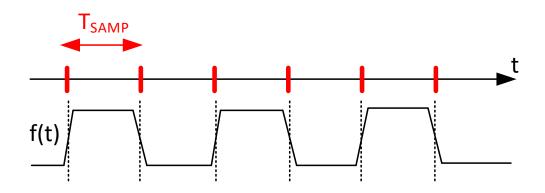
 $\xrightarrow{l_{SAMP}}$

May help a lot ! Use Strobe Period function if available in simulator

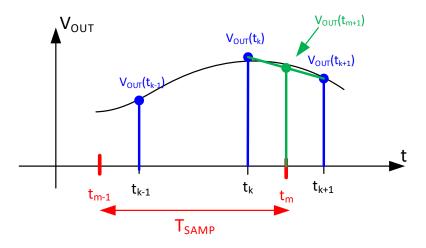
Add noninteracting waveform with steep slope at desired transition points
 May also help a lot ! Forces some time
 stepping algorithms to take sample near
 sample points

If interpolation is a problem, what can be done about it

• Add noninteracting waveform with steep slope at desired transition points



Transient Simulation For Spectral Characterization



Errors associated with interpolation $V_{OUT}(t_k)$

Will consider example using Spectre Do not know what the interpolation algorithm is Will not include any energy storage elements

Spectre Limitations in Spectral Analysis

Thanks to Xilu Wang for simulation results

- Normal Transient Analysis
- Strobe Period Timing
- Coherent Sampling

Simulation Conditions

V(t)=sin(2*π*50t) 11 periods Coherent Sampling

Number of Samples:

- 512
- 4096

Type of Samples:

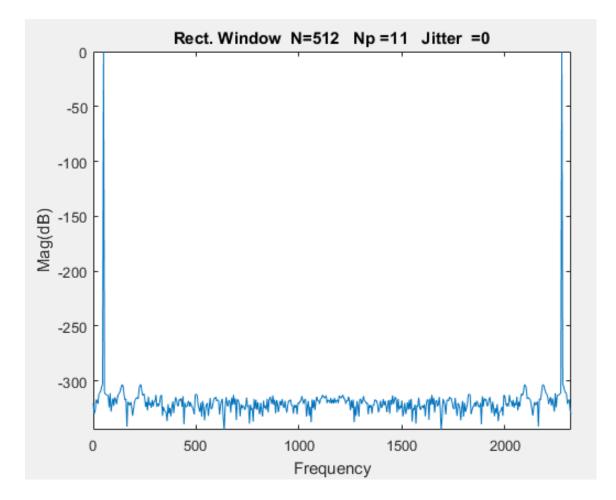
- Standard Sweep
- Strobe Period Sweep

512 Samples with Standard Sweep

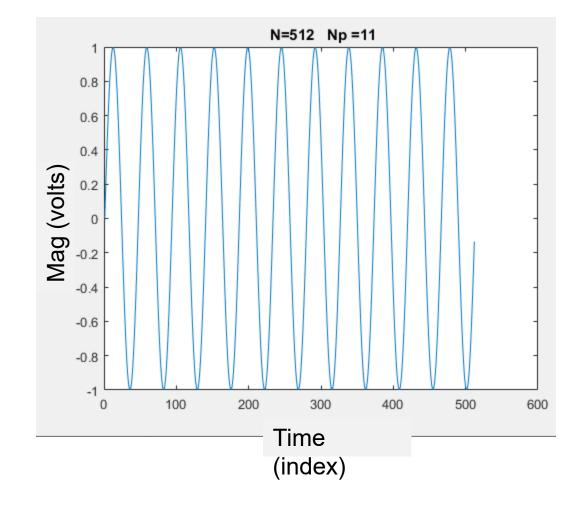
```
V(t) = sin(2^*\pi^*50t)
```

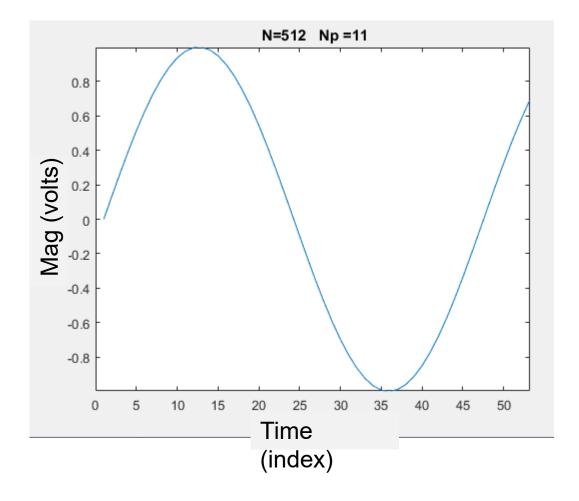
11 periods Coherent Sampling

For reference: Results obtained with MatLab for N=512



512 Samples with Standard Sweep





Pyyt1 =	ĺ
Columns 1 through 12	
-107.8981 -94.1331 -108.0317 -98.4157 -108.4194 -94.7571 -108.9965 -109.0037 -109.6020 -105.0095 -110.0367 -	0.0025
Columns 13 through 24	
-110.1847 -112.5300 -110.0274 -124.3662 -109.6023 -95.7592 -109.0660 -108.3765 -108.6183 -96.3597 -108.3281 -10	1.9470
Columns 25 through 36	
-108.2245 -127.5677 -108.3644 -92.2404 -108.7400 -115.5801 -109.2418 -106.8007 -109.7118 -79.7378 -109.9937 -11	.1.7277
Columns 37 through 48	
-109.9798 -111.2019 -109.6609 -95.7148 -109.1668 -108.6139 -108.7231 -95.8926 -108.4382 -91.2831 -108.3050 -11	0.9404

Columns 49 through 60

-108.3530 -92.7636 -108.6349 -115.7449 -109.1516 -112.1106 -109.8730 -84.9671 -110.7375 -108.1262 -111.5945 -104.6449

Columns 61 through 72

-112.1962 -95.5508 -112.3197 -108.1874 -112.0368 -91.3543 -111.6457 -95.5037 -111.3708 -107.0414 -111.3212 -93.7515

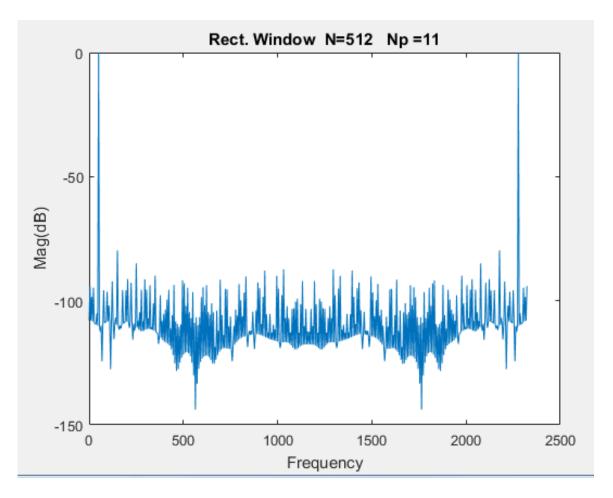
Columns 73 through 84

-111.5009 -110.5545 -111.8098 -101.0709 -112.1458 -89.9120 -112.5548 -112.9274 -113.1741 -117.4284 -114.0466 -97.7820

Columns 85 through 96

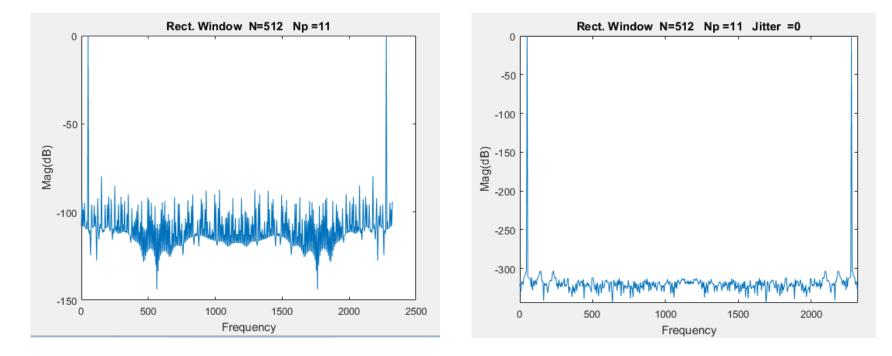
-115.0135 -108.1029 -115.8627 -105.3494 -116.4956 -103.5153 -116.9316 -99.5311 -117.3540 -95.6142 -118.0994 -111.2058 Columns 97 through 108

-119.5251 -105.8620 -121.8988 -93.6210 -125.2388 -108.3341 -128.2779 -109.3118 -127.5511 -110.5460 -124.9168 -109.4982



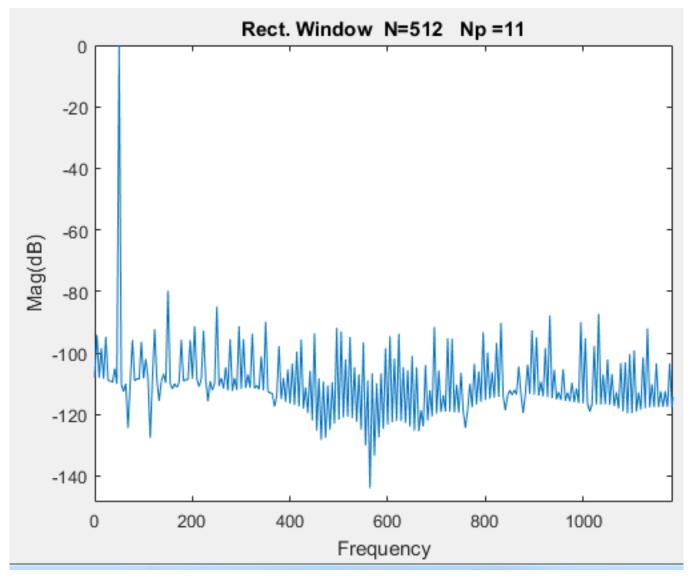
- Note dramatic increase in noise floor
- Note what appear to be some harmonic terms extending above noise floor

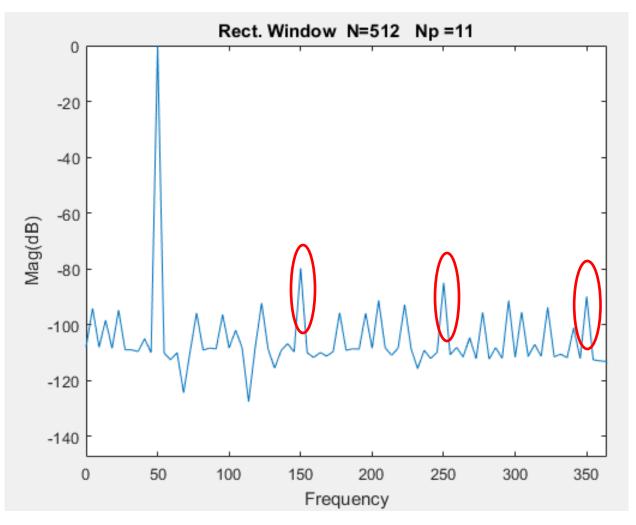
MatLab comparison: 512 Samples with Standard Sweep



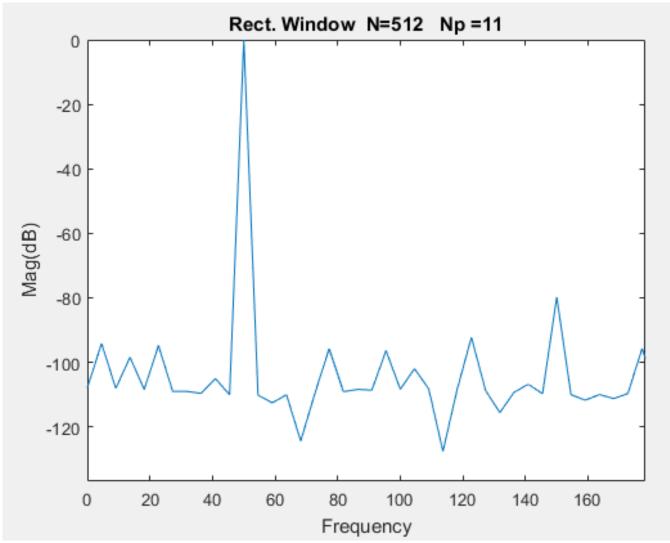
Spectre Results

MatLab Results





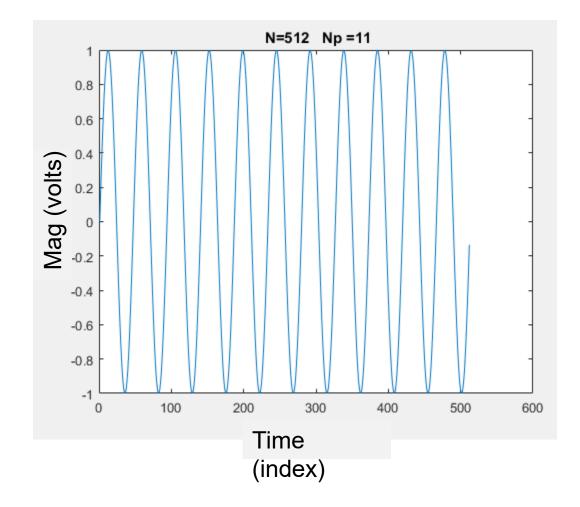
Note presence of odd harmonics in spectrum

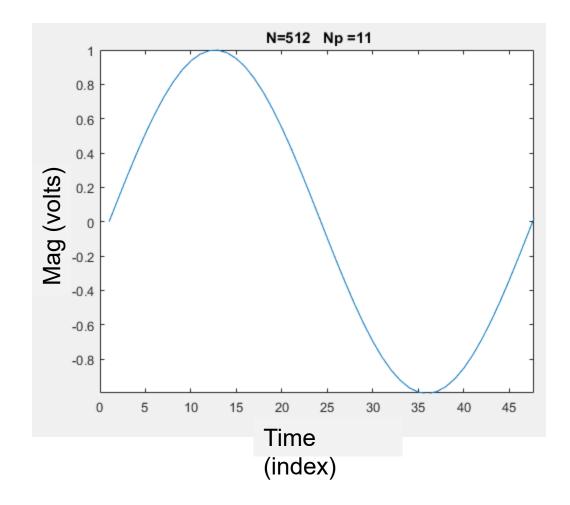


512 Samples with Strobe Period Sweep

```
V(t) = sin(2^*\pi^*50t)
```

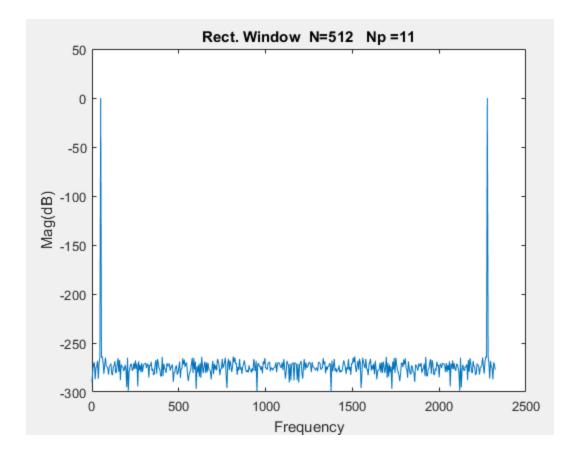
11 periods Coherent Sampling



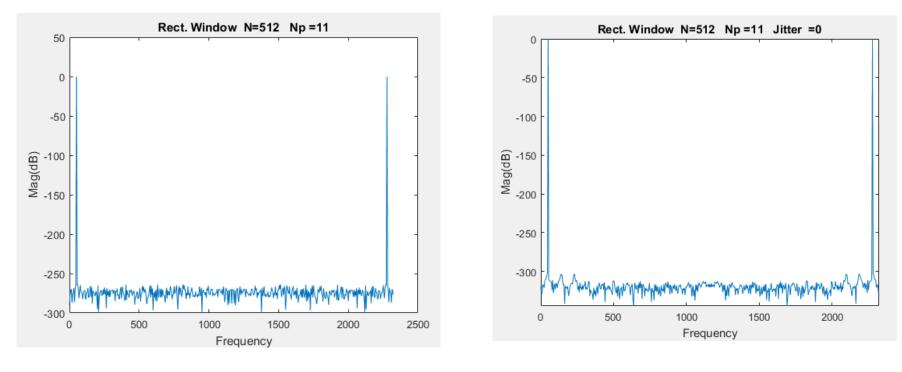


Pyyt2 = Columns 1 through 12 -289.9823 -277.1621 -271.8971 -269.7867 -287.1463 -274.9517 -274.1616 -268.2808 -286.3367 -270.6890 -264.2517 0.0000 Columns 13 through 24 -264.9125 -263.7218 -269.4627 -281.3076 -273.7005 -264.8333 -273.1021 -274.2804 -275.7987 -282.2465 -273.4191 -272.4758 Columns 25 through 36 -270.9356 -281.3558 -282.8219 -274.2676 -273.4832 -268.4204 -280.8477 -279.3164 -270.8593 -265.4445 -279.4813 -267.3563 Columns 37 through 48

-288.0473 -271.6637 -274.6875 -274.0074 -278.3424 -277.6395 -272.2091 -276.9768 -295.2068 -265.0774 -298.7341 -280.0345

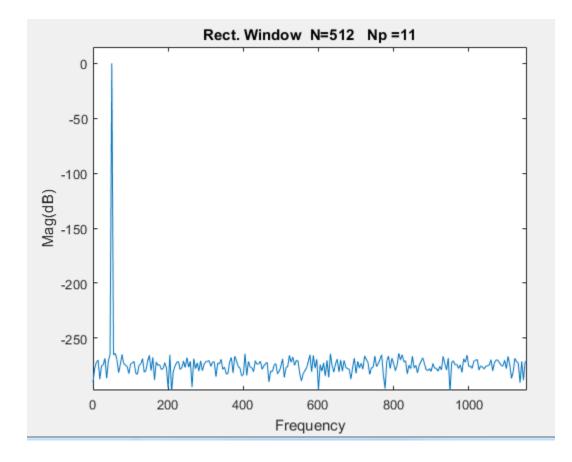


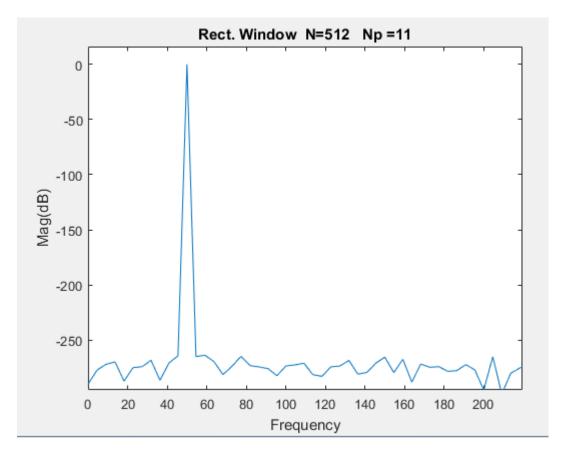
MatLab comparison: 512 Samples with Strobe Period Sweep



Spectre Results

MatLab Results

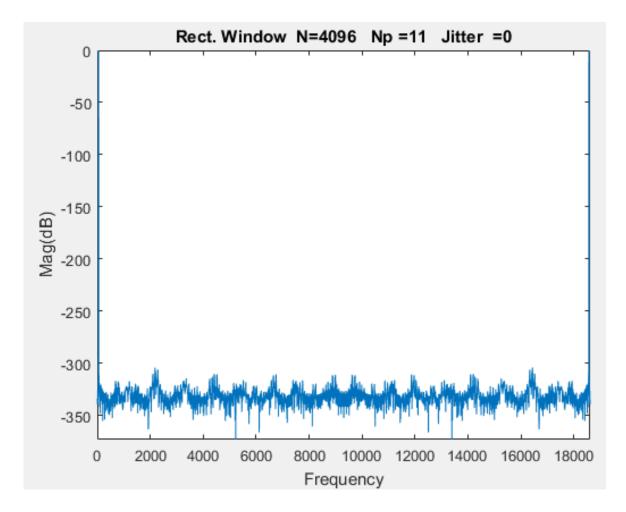


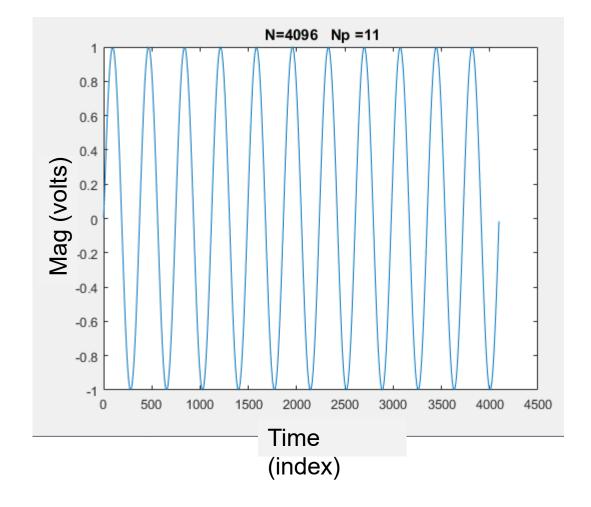


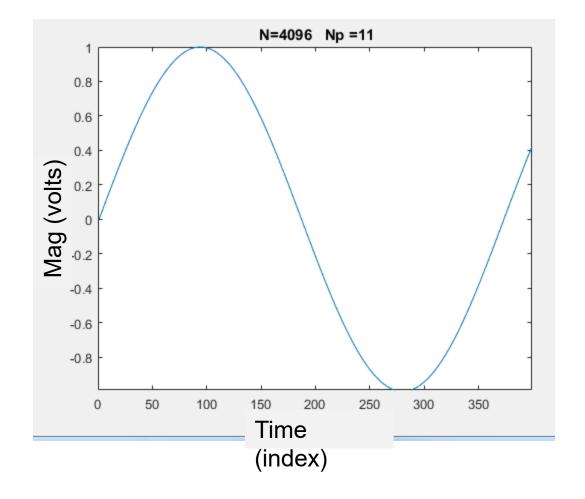
```
V(t) = sin(2^*\pi^*50t)
```

11 periods Coherent Sampling

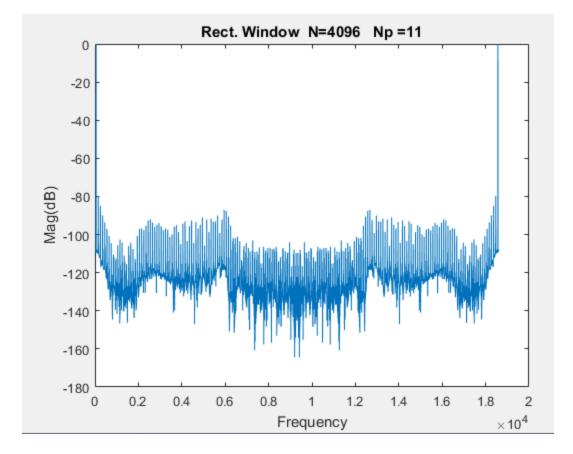
For reference: Results obtained with MatLab for N=4096



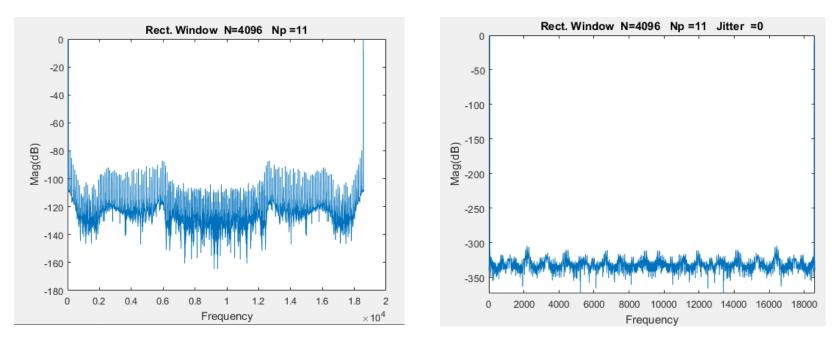




Pyyt3 =	c
Columns 1 through 12	
-108.3243 -108.1538 -108.2707 -108.0618 -108.1535 -108.0412 -108.0422 -109.2666 -107.9762 -107.8815 -107.9734	-0.0024
Columns 13 through 24	
-108.0437 -108.0723 -108.1927 -109.4684 -108.4265 -108.3864 -108.7503 -107.7815 -109.1369 -109.1277 -109.4911 -10	09.7293
Columns 25 through 36	
-109.7098 -108.8871 -109.7944 -109.4286 -109.8171 -108.5378 -109.8456 -109.8612 -109.9177 -79.7470 -110.0501 -12	10.1301
Columns 37 through 48	
-110.2518 -104.6517 -110.5298 -110.8421 -110.8907 -111.4034 -111.3159 -111.0945 -111.7096 -111.7185 -111.9500 -1	11.0991

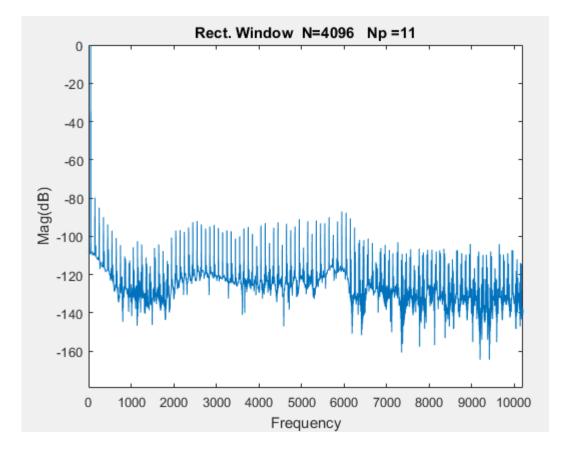


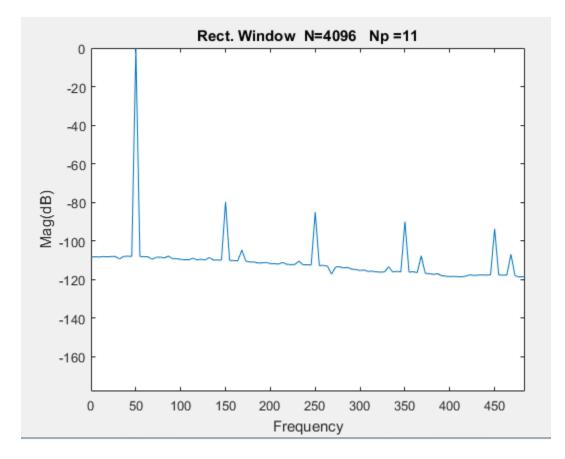
Comparison 4096 Samples with Standard Sweep



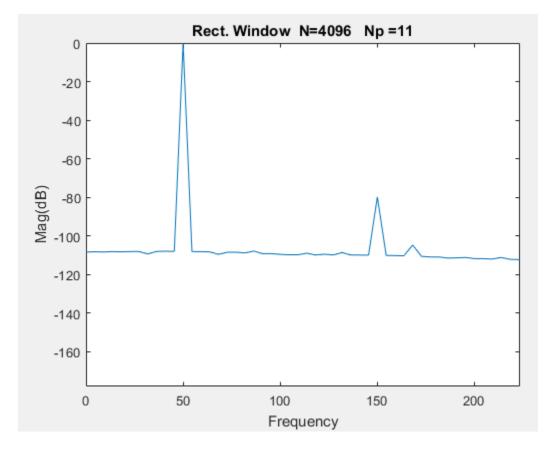
Spectre







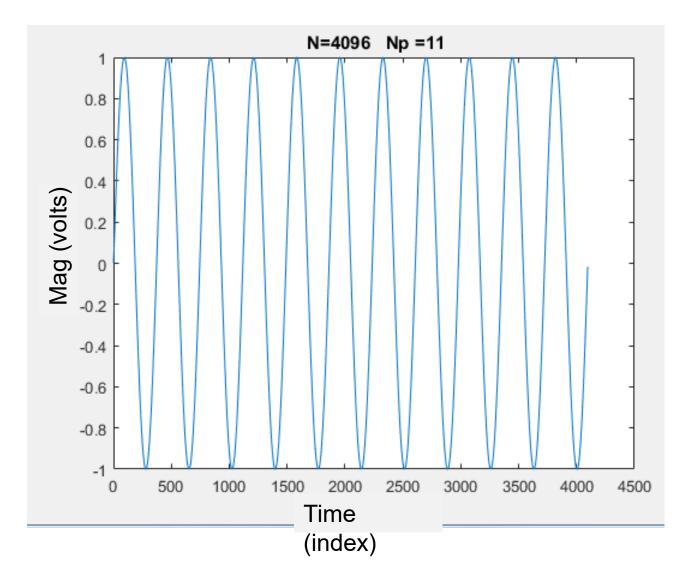
Note presence of odd harmonics in spectrum

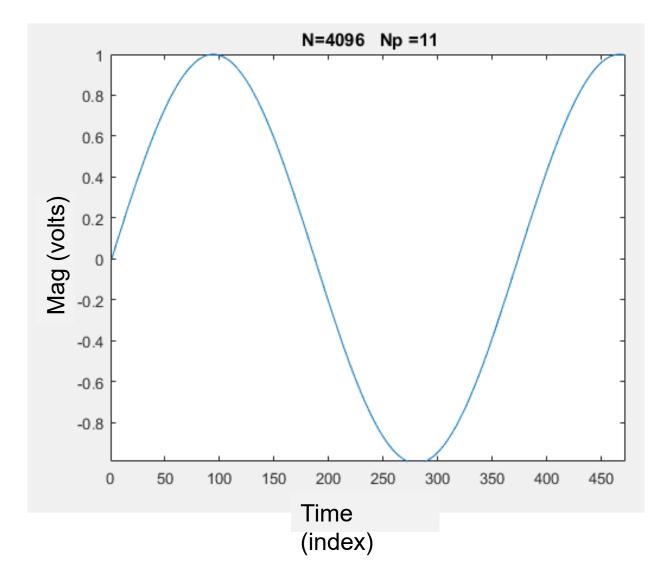


4096 Samples with Strobe Period Sweep

```
V(t) = sin(2^*\pi^*50t)
```

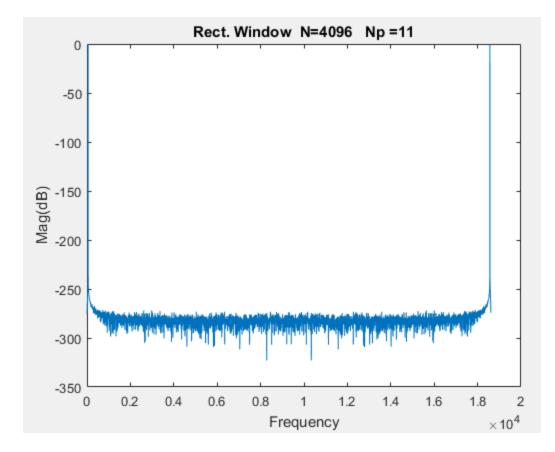
11 periods Coherent Sampling



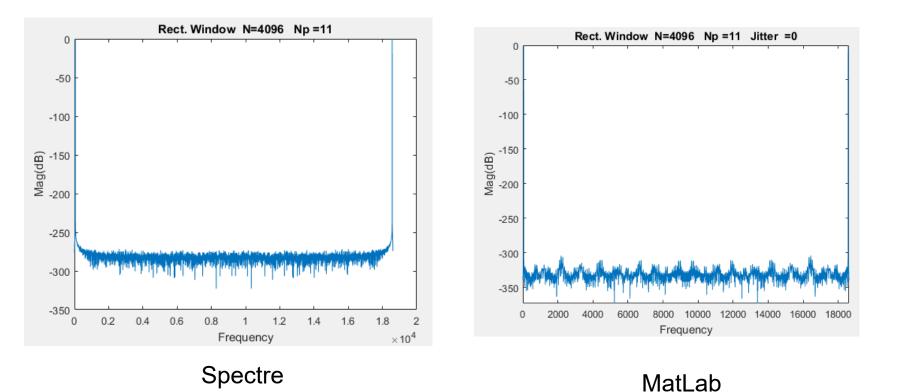


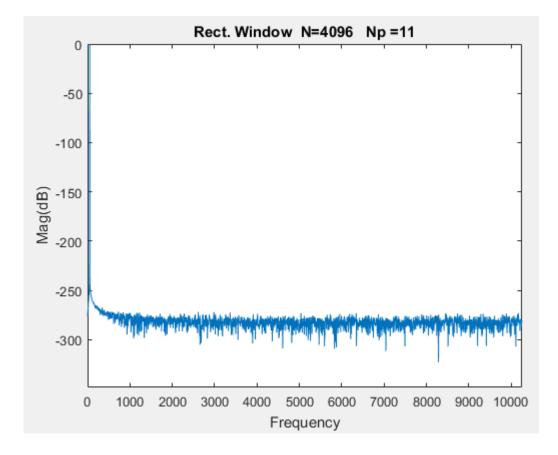
Pyyt4 = Columns 1 through 12 -275.7993 -274.2288 -271.2122 -266.4879 -261.9356 -260.8993 -256.6778 -254.4684 -252.1418 -247.4997 -238.6334 -0.0000 Columns 13 through 24 -237.9355 -245.9934 -249.3333 -250.9084 -252.6585 -254.7659 -255.1826 -256.4114 -256.4550 -258.0311 -258.5182 -259.4258 Columns 25 through 36 -260.1189 -260.6618 -260.7491 -261.8162 -261.6129 -262.3357 -262.2738 -263.3625 -264.1235 -263.3313 -262.6442 -264.9796 Columns 37 through 48

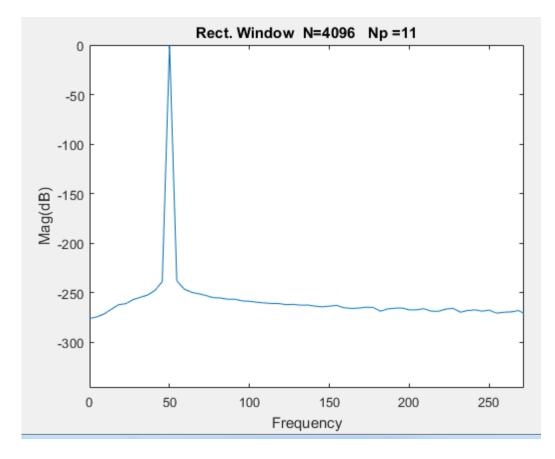
-265.6690 -265.3833 -264.5215 -264.5995 -268.4617 -266.2074 -265.4619 -265.3134 -267.1584 -267.0717 -265.9300 -268.4336



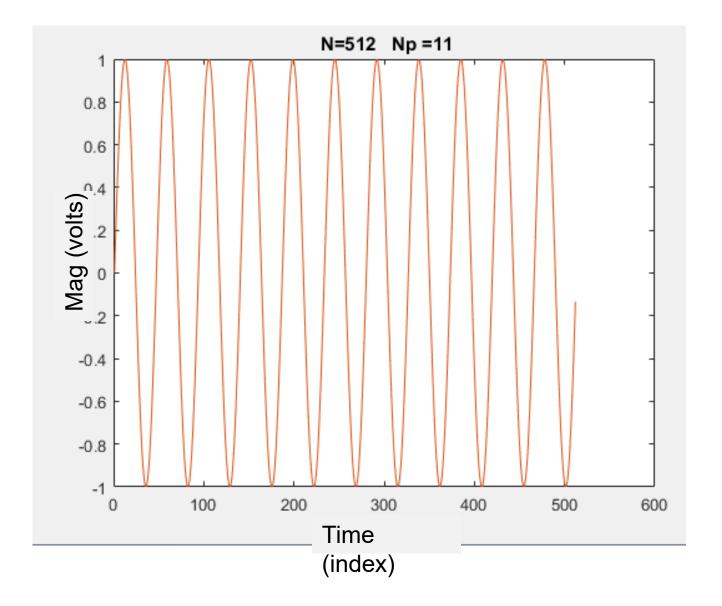
Comparison 4096 Samples with Strobe Period Sweep



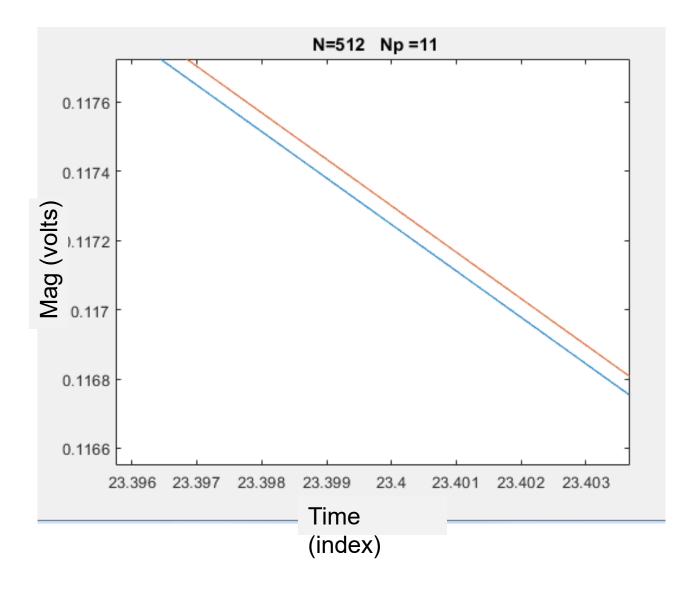


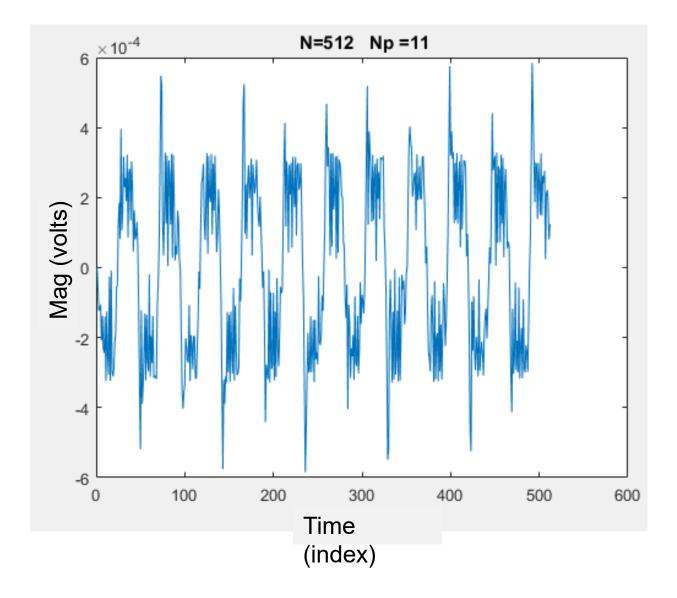


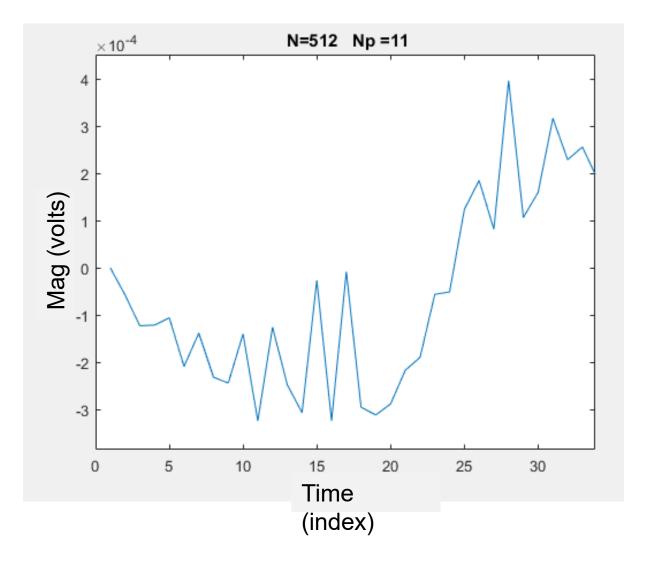
Superimposed Standard/Strobe Sweep

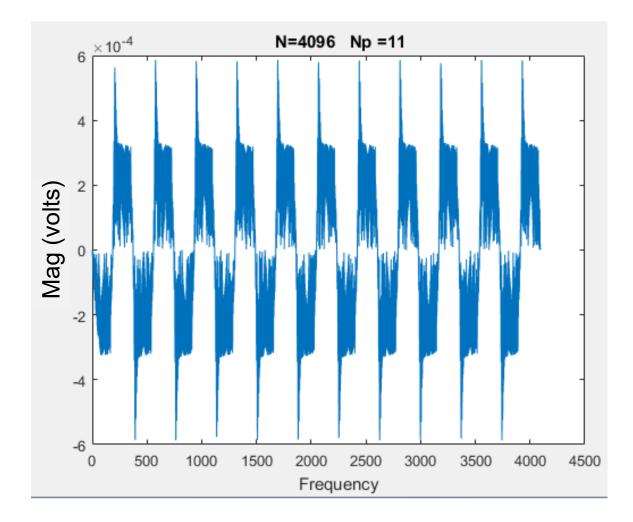


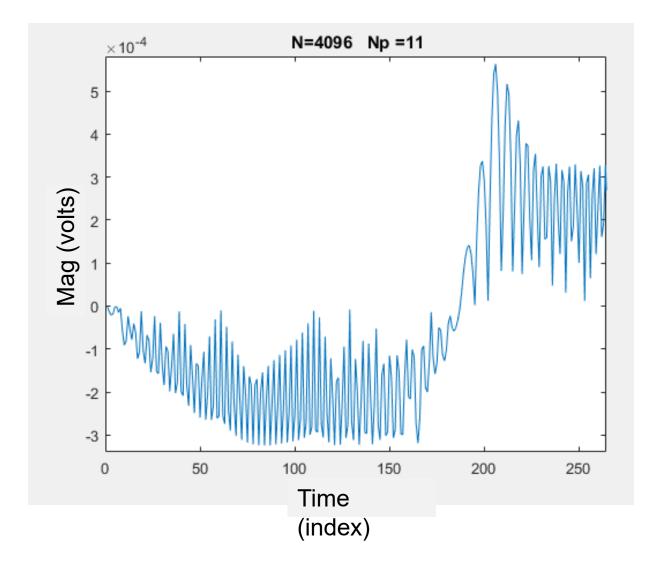
Superimposed Standard/Strobe Sweep











Addressing Spectral Analysis Challenges

- Problem Awareness
- Windowing and Filtering
- Post-processing

Problem Awareness

THEOREM: Consider a periodic signal with period T=1/f and sampling period T_S=1/f_S. If N_P is an integer, x(t) is band limited to f_{MAX} , and f_s >2 f_{max} , then

 $|A_{m}| = \frac{2}{N} |X(mN_{P} + 1)|$ $0 \le m \le h - 1$

and X(k) = 0 for all k not defined above

where $\langle X(k) \rangle_{k=0}^{N-1}$ is the DFT of the sequence $\langle x(kT_s) \rangle_{k=0}^{N-1}$

N=number of samples, N_P is the number of periods, and h = Int $\left(\frac{f_{MAX}}{f} - \frac{1}{N}\right)$

- Hypothesis is critical
- Even minor violation of the premise can have dramatic effects
- Validation of all tools is essential
- Learn what to expect

Filtering - a strategy to address the aliasing problem

- A lowpass filter is often used to enforce the band-limited requirement if not naturally band limited
- Lowpass filter often passive
- Lowpass filter design often not too difficult
- Minimum sampling frequency often termed the Nyquist rate.

End of Lecture 6